

# Active and passive tracing of non-metallic inclusions in steel using rare earth elements

<u>Christoph Walkner<sup>1\*</sup>, Kathrin Thiele<sup>2</sup>, Susanne K. Michelic<sup>2</sup>, Thomas C. Meisel<sup>1</sup>, Sergiu Ilie<sup>3</sup>, Roman Rössler<sup>3</sup></u> and Thomas Prohaska<sup>1</sup> \*Christoph.walkner@unileoben.ac.at

<sup>1</sup> Montanuniversität Leoben, Department General, Analytical and Physical Chemistry, Chair of General and Analytical Chemistry, 8700 Leoben, Austria

<sup>2</sup> Montanuniversität Leoben, Christian Doppler Laboratory for Inclusion Metallurgy in Advanced Steelmaking, 8700 Leoben, Austria

<sup>3</sup> voestalpine Stahl GmbH, 4020 Linz, Austria

#### Introduction

Non-metallic inclusions (NMIs) negatively affect both physical and corrosive properties of steels, to the point of material failure (Fig. 1). In addition, clogging, i.e. the aggregation of non-metallic particles during the steel casting process, can further reduce steel quality or even interrupt the process (Fig. 2). [1] Within the present study, we investigated the formation of NMIs and clogging in titanium stabilised ultra-low carbon (Ti-ULC) steel, a material mainly used for automobile panels (Fig. 3).



## **Results & Conclusions**

- Results gained using both the active and passive tracing approach consistently link the clogging material from the SEN to the aluminium added in the deoxidation step.
- Agglomeration of aluminium oxide particles is the main reason for clogging during the Ti-ULC steel casting process.

### **Steel production process**











1: SEM image of a non-Fig. metallic inclusion (NMI) in steel which has caused cracking.

Fig. 2: Clogging at the Fig. 3: Automobile panels as an example for the use of Ti-ULC steel. [2] submerged entry nozzle (SEN)

## **Sample preparation for ICP-MS analysis**



Fig. 5: Schematic of the steel production process, Material flows and sampling strategy.

#### Active tracing

In the active tracing approach, La and Ce are added to the steel melt on an industrial scale. [4] Due to their high oxygen affinity, these elements are quickly transferred into oxide phases, such as NMIs consisting mainly of AI oxide, following equation 1:



#### **Passive tracing**

In the passive tracing approach, distribution patterns (chondrite normalised mass fractions [3]) of the rare earth elements (REE) in clogging material from the SEN and potential source materials are compared.



**Fig. 4**: Chondrite normalised REE mass fractions determined using ICP-MS after Na<sub>2</sub>O<sub>2</sub> sintering or HCI/HNO<sub>3</sub> digestion in SEN clogging material and reference samples. Values for Pm (\*), which does not occur naturally, were interpolated between Nd and Sm.

 $2 \operatorname{Al}_2 \operatorname{O}_3 + 2 \operatorname{La} \rightleftharpoons \operatorname{La}_2 \operatorname{O}_3 \cdot \operatorname{Al}_2 \operatorname{O}_3 + 2 \operatorname{Al}_2 \operatorname{O}_3$ (1)

Steel samples from two heats (using the same SEN) were analysed using ICP-MS (Fig. 6), heat 1 with La addition and heat 2 with Ce addition (~40 mg La/Ce per kg steel). The clogging layer formed at the SEN was investigated using SEM/EDS, as were individual NMIs found in the steel slabs (Fig. 7).



Fig. 6: La and Ce mass fractions in steel samples taken throughout the process, determined using ICP-MS after acid digestion.



- Similar trends are visible in the REE patterns of auxiliary material II (sliding gate sand) and the clogging sample.
- Both AI granules (added for deoxidation) and clogging sample have high Nd and low Eu contents.
- Clogging formation can be explained by a combination  $Al_2O_3$  (oxidised Al granules) and silicate components of the sliding gate sand.

## References

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Fig. 7: Left: SEM/EDS element mappings of the clogging layer deposited at the SEN Right: SEM/EDS image and elemental mappings of a La containing NMI

- La and Ce were found in in the SEN clogging layer, in individual NMIs in steel slabs, and in bulk analyses of steel samples (most likely also present in NMIs).
- There is only a short window of time in which REE are available for reactions as in equation 1, before they are oxidised and transferred into the slag phase.
- Therefore, the oxide material building up the clogging layer (and NMIs) must have already been present at the time of La/Ce addition, leaving  $AI_2O_3$  generated from added AI as the most likely source.



Chair of General and Analytical Chemistry | Franz-Josef-Straße 18, 8700 Leoben, Austria